Evaluation of Stripping Potential Tests for Bituminous Concrete

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Background

Moisture Susceptibility – Reduction in strength of the asphalt pavement in presence of moisture.



Source: Veeraragavan (2020)

Source: Williams (2010)

Source: Colorado Pavement Solution (2019)

Longitudinal Cracks

Alligator Cracks



Raveling



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Moisture Susceptibility Tests



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Results – Boiling Water Test

Queantifying Respition Boiling Water Test

Weight Loss		LOV. KAL		Sample ID	Mix	Box	Mix	Sample	Asphalt Retained
				odnipie ib	Design	Numbering	Туре	Date/Time	after boiling (%)
		Drv Mass	Drv Mass	Percent Loss	9-752	20-001	IIS	NA	90-100
B.C		Defense	After		9-752	20 002 C	eliab	le due to	90-100
wiixture	Aggregate Type	Betore	Atter	In Asphalt	9-752	20-003 n	sian	ificant	90-100
		Boiling (g)	Boiling (g)	Binder (%)	9-752	20-004	IIS	NA	90-100
1	Prone	245.2	244.2	0.4	9-752	20-005			90-100
2	Non-Prone	255.8	255	0.3	9-752	20-006		St _{NA}	90-100
		23 C. 24		Pserven209H054644	19-752	NA	IIS	09/17/20-12:33	90-100
				Pserven209H054644	19-752	NA	IIS	09/17/20-09:54	90-100
Specific G	ravity		Carlos S.	Pserven209H054644	19-752	NA	IIS	09/17/20-08:40	90-100
		1000		Burlington STP	IVS	NA		e as spe	90-100
Specific gr	avity of bitumer	n falls within	the range of	0.97 to 1.02 at Burlington STP		Ngra	vity	of aspha	t i S 0-100
(CIVICCONC	epts; 2022)	A Provide State		Burlington STP	IVS	elos	e ^r to	that ∕of v	
200/				Burlington STP	IVS	NA	IVS	NA	90-100
30% KAP		20% RAP		Burlington STP	IVS	NA	IVS	NA	90-100
				NA	SP-18751	NA	IVS	11/03/20-10:30	90-100



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Conclusions and Recommendations

- Plant produced HMA mixtures have low moisture susceptibility based on the ASTM D3625 and AASHTO T283. More robust test such as MiST could be useful.
- Adding 10% additional RAP (i.e. up to 30%) to the HMA mix showed same level of asphalt binder retainment as the plant produced HMA mix with 20% RAP.
- Quantification of ASTM D3625 is unreliable due to insignificant difference in weight loss and specific gravity of asphalt and water.
- □ TSR > 0.8 for all the mixtures. One extra wet cycle not enough to induce additional damage. More laboratory testing needed to determine the minimum cycles of Lottman conditioning.



Thank you for your attention



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Additional Slides



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Comparison between Joint and Regular Cores



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Results – Boiling Water Test

Effect of RAP

Mix #	Aggregate type	RAP content	ASA	Production
1	Prone	30	Yes	UVM Lab
2	Non-prone	20	Yes	Plant produced

Job-Mix Formula (Provided by Dr. Anderson)

S.N.	AC Components	Percentage by weight (%)
1	Washed Stone Screening	37.5
2	Natural Sand	12.2
3	3/8 "Minus Course Aggregate (Prone/ Non- Prone)	<u>25.4</u> 15.4
4	RAP	20 20
5	Asphalt Binder	4.9



LU/ KMF



30% RAP

20% RAP



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Results – Boiling Water Test

Quantifying Result of Boiling Water Test

Weight Loss

Mixture	Aggregate Type	Dry Mass Before	Dry Mass After	Percent Loss in Asphalt	
		Boiling (g)	Boiling (g)	Binder (%)	
1	Prone	245.2	244.2	0.4	
2	Non-Prone	255.8	255	0.3	

Unreliable due to insignificant difference in mass lost

Specific Gravity

□ Specific gravity of bitumen falls within the range of 0.97 to 1.02 at 27 °C (Civicconcepts, 2022)

Unreliable as specific gravity of asphalt is close to that of water



Effect of Compaction – Joint Cores Vs Regular Cores



Percent Compaction, P_c (%)

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Materials



Asphalt Concrete







Plant Produced HMA

Raw Aggregates and RAP

Asphalt Binder and ASA

Asphalt Cores



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Storage in the lab



Plant produced HMA and Raw Aggregates

Asphalt core boxes on a flat surface



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Test Procedure

Boiling Water Test – ASTM D3625



for 2 hours

Boil for 10 mins

Let it cool at room temperature

Visually evaluate the binder retained on aggregate

Also, measure weight



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Test Procedure – Modified Lottman Test





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Test Procedure – Wet Conditioning for Lottman Test

Vacuum for 5 mins











Freeze @ -18 °C (0 °F) for 16 hours



Loading @ 50 mm/min (2 in/min)











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Test Procedure – Dry Conditioning for Lottman Test

Oven @ 25 °C for 1 hour prior to test







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Measure the peak strength





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Calculation

□ Calculate the indirect tensile strength of all the cores:

Tensile Strength, S_t (in psi) = $\frac{2*P}{\pi tD}$

P = Maximum peak strength, lbft = Average thickness of core, inD = Core diameter, in

□ Determine average peak strength for the sub-group i.e., dry and conditioned

□ Calculate the Tensile Strength Ratio (TSR):

 $TSR = \frac{Avg.Tensile\ Strength\ of\ Conditioned\ Cores}{Avg.Tensile\ Strength\ of\ Dry\ Cores}$

AASHTO T-280 threshold of TSR is 0.8

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Results – Boiling Water Test

Sensitivity of ASA



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Stripping Prone Aggregate

S.N	Load (N)	S _{t, cond.} (kPa)	Avg. S _t	Туре	TSR
1	7892.50	0.66			
2	7359.10	0.62	0.65	Cond.	
3	8047.90	0.67			0.75
4	11841.00	0.99			0.75
5	9294.00	0.78	0.87	Dry	
6	9997.10	0.84			

Stripping non-prone Aggregate

S.N	Load (N)	S _{t, cond.} (kPa)	Avg. S _t	Туре	TSR
1	7033.90	0.59		Cond.	0 00
2	8497.50	0.71	0.69		
3	9073.90	0.76			
4	9989.90	0.84			0.88
5	8827.60	0.74	0.78	Dry	
6	9140.90	0.77			

Showed promising result to identify the moisture susceptible mixture even in the presence of ASA

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Effect of Compaction – Groton-Newbury Project (Dry Vs Wet Cores)





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Effect of Compaction – Richford-Jay Project (1 cycle Vs 2 cycles)



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Effect of Compaction – Cavendish-Weathersfield Project (1 cycle Vs 2 cycles)





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Effect of Core Thickness





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References

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Void Ratio and Degree of Saturation of the samples

Richford-Jay Project



Double Cycle of Wet Conditioning



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Texas Rating Board

Texas Boiling Test Rating Board % Asphalt Retained

30.00 01.0



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Recommendations

- Due to inaccuracy of MRD-1 and MRD-10 tests, other tests such as boiling water tests), modified Lottman test, Hamburg wheel tracking (AASHTO T 324), MiST etc. are recommended.
- Other quantifying techniques such as image processing, color analyzing methods of pre- and postboiled samples.
- More testing, especially quantitative tests such as modified Lottman test, Hamburg wheel tracking test, is required to justify the use of 30% RAP in the HMA mixtures.
- □ More testing under laboratory conditions to determine the minimum number of lottman conditioning is recommended to develop a robust specification for testing moisture susceptibility of the HMA mixtures.
- The joint cores showed lower compaction level and hence lower tensile strength than the regular cores. More compactive effort on joints is recommended.



Schedule of Deliverables

Project Start Date: 7/27/2020

End Date: 6/30/2022

Period	Deliverables	Status
AugSept. 2020	Deliverable 1 – literature review to identify a quantitative measure to improve the effectiveness of the ASTM D3625 anti-strip test	Delivered
OctDec. 2020	Deliverable 2 – Preliminary report on progress of preparing different mixes	Delivered
JanMarch 2021	Deliverable 3 – Preliminary report on progress of stripping resistance evaluation according to ASTM D3625 testing procedure	Delivered
April-June 2021	Deliverable 4 – Preliminary report on stripping risk posed by using RAP and emulsion in the mix design	Delivered
July-Sept. 2021	Deliverable 5 – 5.1 –Report on assessment of stripping potential and ASA performance supplied by different HMA producers, evaluation of the ASTM D3625 for use in Vermont, and required updates to current VTrans testing procedure	Delivered
OctDec. 2021	5.2 – Preliminary report on the impact of wet versus extended wet conditioning on peak strength and TSR	Delivered
JanMarch 2022	5.3 – Preliminary report on the trends of variation of tensile strength values with density for cores subjected to wet versus extended wet conditioning	Delivered
April-June 2022	Deliverable 6 – Technology Transfer deliverables: draft final report including benefits quantification and implementation guidelines, final poster and fact sheet, final presentation to the TAC, and final report including any TAC comments.	Delivered



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